

## Effect of Thermal and Mechanical Aging on Flexural Strength of Zirkonzahn and Mamut Zirconia Ceramics

<sup>1</sup>Kasra Tabari <sup>2</sup>Zahra Jaber Ansari \*<sup>3</sup>Manousha Amiri Siavashani <sup>4</sup>Solmaz Eskandarion

<sup>1</sup>Assistant Professor, Dept. of Restorative Dentistry, School of Dentistry, Shahid Beheshti University of Medical Sciences, Tehran, Iran.

<sup>2</sup>Associate Professor, Dept. of Restorative Dentistry, School of Dentistry, Shahid Beheshti University of Medical Sciences, Tehran, Iran.

<sup>3</sup>Assistant Professor, Dept. of Restorative Dentistry, School of Dentistry, Qom University of Medical Sciences, Qom, Iran. E-mail: manusha\_amr@yahoo.com

<sup>4</sup>Assistant Professor, Dept. of Dental Materials, School of Dentistry, Shahid Beheshti University of Medical Sciences, Tehran, Iran.

### Abstract

**Objective:** Despite the high strength of zirconia restorations, aging in the oral environment and masticatory loading may result in transformation of tetragonal to monoclinic phase and decrease their strength. Statements in this regard are controversial. This study sought to compare the flexural strength (FS) of Zirkonzahn (ZirkonZahn, Cercon, Ceramill) and Mamut (Dubai Medical Equipment LLC, Dubai, UAE) zirconia ceramics and assess the effect of thermal and mechanical aging on their FS.

**Methods:** In this *in vitro* experimental study, 40 bar-shaped specimens measuring 20×5×2 mm were cut from Zirkonzahn and Mamut zirconia blocks and polished. Specimens in the aging groups were subjected to thermocycling (12,000 cycles, 5-55°C, dwell time of 20 seconds). Next, they were subjected to mechanical stress in a chewing simulator (40,000 cycles, 200N force). The three-point flexural strength (TPFS) was determined in megapascal (MPa) using a Universal Testing Machine at a crosshead speed of 0.5 mm/min. Data was analyzed using two-way ANOVA.

**Results:** The mean and standard deviation (SD) of TPFS of Zirkonzahn and Mamut specimens in the no aging group was 809.57 (205.95) and 708.53 (158.72) MPa, respectively. These values were 810.53 (158.96) and 839.06 (217.49) MPa for the Zirkonzahn and Mamut specimens subjected to aging, respectively. Type of zirconia (Zirkonzahn or Mamut) and exposure to aging process ( $p=0.27$ ) had no significant effect on TPFS of specimens.

**Conclusion:** Within the limitations of this study, the results showed that the process of aging did not decrease the TPFS of Zirkonzahn and Mamut specimens. Thus, these ceramics may be successfully used in the clinical setting.

**Key words:** Aging, Ceramic, Strength, Zirconia.

**Please cite this article as:**

Tabari K, Jaber Ansari Z, Amiri Siavashani M, Eskandarion S. Effect of Thermal and Mechanical Aging on Flexural Strength of Zirkonzahn and Mamut Zirconia Ceramics. *J Dent Sch* 2014; 32(3): 132-138.

Received: 17.08.2013

Final Revision: 16.12.2013

Accepted: 08.02.2014

### Introduction:

Zirconia-based ceramics are the most-recent generation of high-strength ceramics. Favorable mechanical properties, high esthetics, excellent biocompatibility, insignificant plaque accumulation and low thermal conductivity are among the advantages of zirconia ceramics. All these factors play a role in selection of these

ceramics for esthetic tooth restorations (1).

Mechanical properties of dental materials such as their strength are the main parameters taken into account when assessing the possible applications and clinical limitations of dental restorations. Despite the favorable mechanical properties of zirconia ceramics, the surface of zirconia specimens may undergo changes. Occasionally, in humid environments at

relatively low temperatures, the tetragonal phase of zirconia may transform into the monoclinic phase (2). This phenomenon, known as the low temperature degradation, is related to the partial stability of the tetragonal phase at room temperature and may lead to the formation of small and large cracks, decrease strength and impair mechanical properties of zirconia (3-5). This mechanism occurs very slowly in the oral environment but may decrease the strength and density of zirconia restorations (6, 7). Moreover, the strength may further decrease due to cyclic stresses attributed to the masticatory loading in the clinical setting (8, 9). Thermal stresses may also decrease the zirconia strength and create strain inside the ceramic materials (10, 11). Some studies have demonstrated that the process of aging of yttria-stabilized zirconia specimens at low temperatures causes the transformation of tetragonal to monoclinic phase and creates small cracks in the zirconia structure (12). The speed of phase transformation is related to factors such as temperature, size of grains, dopant concentration (13) and surface polishing of specimens (14). Rapid phase transformation leads to the destruction of ceramic specimens and decreases their strength.

Dopants, available in the form of solid solutions, are added to zirconia ceramics in small amounts to change their chemical properties. Dopants like silica and alumina directly alter the morphology, substructure and stability of zirconia ceramics (15, 16). Ceria, also added to zirconia ceramics, plays a role in the process of sintering and improves resistance to aging (17, 18).

Due to functional loading in the oral environment, zirconia-based restorations may develop fatigue in spite of high strength (19). Over time, these stresses accumulate and cause tiny defects (20) and small cracks (21) in the material.

The process of aging may affect the strength of dental ceramics (22). Thus, it is necessary to assess the effect of aging on the strength of

zirconia ceramics. Considering the existing concerns regarding the adverse effects of aging on mechanical properties and strength of zirconia ceramics, this study aimed to compare the FS of Zirkozahn and Mamut zirconia specimens and evaluate the effect of thermal and mechanical aging on their FS.

## Methods:

This was an *in vitro*, experimental study. Specimens were prepared in a laboratory and those with inaccurate dimensions were excluded and replaced with accurate ones. Specimens were evaluated in four groups of 10. Sample size was calculated to be 10 specimens in each group by a statistician according to similar previous studies (22, 23, 24). Specimens were randomly divided into four groups of Zirkozahn and Mamut zirconia specimens with and without aging.

Twenty specimens were fabricated of each type of zirconia according to the manufacturers' instructions. Bar-shaped specimens, 4 (0.25) mm in width,  $1.2 \pm 0.2$  mm in thickness and 20mm in length, were cut from ceramic blocks via the machining process using 30-40 $\mu$ abrasive diamond discs. Specimens were then polished with 15-20 $\mu$  diamond discs and the opposing surfaces were paralleled. Next, all Zirkozahn and Mamut specimens were rinsed with distilled water to remove any remaining debris. Zirkozahn and Mamut zirconia specimens in the aging groups were thermocycled (Thermocycler, Dorsa, Iran) for 12,000 cycles. At each cycle, specimens were immersed in a distilled water bath at 5°C for 20 seconds, followed by 20 seconds of dwell time in the air and another 20 seconds in a distilled water bath at 55°C. After thermocycling, bar-shaped specimens were placed in CS-4 chewing simulator (SD Mechatronik, Feldkirchen-Westerham, Germany) to receive 40,000 cycles at a load of 200N=20Kg in order to simulate

masticatory loads in the clinical setting. Three-point flexural strength testing was performed according to ISO6872 standards. This test was performed under dry conditions at room temperature by Universal Testing Machine (Santam, Iran). Bar-shaped specimens were placed on the two jigs of the machine. The jigs had a semi-circle cross-section with 1.6mm diameter. The span length was 15mm. Compressive strength was applied by the upper blade (with a semi-circle cross-section and 1.6mm diameter) from the top at a crosshead speed of 0.5 mm/min in between the two jigs (Figure 1) until fracture.



**Figure 1- Bar-shaped specimen placed on the two jigs. Load was applied from the top by the blade for TPFS testing**

To calculate mechanical parameters by the software of Universal Testing Machine, three

different parameters are defined for each specimen: thickness of specimen, width of specimen and length of specimen. These parameters were accurately measured for each specimen using a digital micrometer (Mitutoyo Ltd., Andover, England) and entered in the software as the characteristics of the specimen. After TPFS testing, the load at failure for each specimen was calculated in MPa and the FS was calculated using the following equation:

$$TPFS = \frac{3wl}{2bd^2}$$

Where w is the load at failure (N), l is the length of span (mm), b is the width of specimen and d is the thickness of specimen (mm)

TPFS data of specimens in different groups were statistically analyzed using two-way ANOVA.

**Results:**

Based on the results, the mean and SD of TPFS of Zirkozahn specimens was 809.57 (205.95) MPa in the no aging and 810.53 (158.96) MPa in the aging group. For Mamut specimens, these values were 708.53 (158.72) MPa and 839.06 (217.49) MPa, respectively (Table 1).

Type of zirconia ceramic (Zirkozahn or Mamut) ( $p=0.54$ ) and the aging process ( $p=0.27$ ) had no significant effect on the FS of specimens. Moreover, the interaction effect of the type of zirconia and aging on flexural strength was not statistically significant ( $p=0.28$ ).

**Table 1- The mean and SD of TPFS of Zirkozahn and Mamut specimens with and without aging**

Group	Aging	Number	mean	SD	Minimum	Maximum
Zirkozahn	Aging	10	810.53	158.96	482.94	1111.64
	No aging	10	809.57	205.95	592.23	1242.65
Mamut	Aging	10	839.06	217.49	572.74	1340.44
	No aging	10	708.53	158.72	461.98	964.49

**Discussion:**

In this study, Mamut and Zirkozahn specimens

were subjected to thermal and mechanical cycles to assess the effect of these processes on TPFS of ceramics. Based on the results, aging or type

of zirconia had no significant effect on FS of specimens. Moreover, the two types of zirconia were not significantly different in terms of FS. The obtained FS values for Zirkozahn and Mamut zirconia were not similar to the values claimed by the manufacturers (1400 and 1100 MPa, respectively). This difference may be explained by the general differences in preparation of specimens, sintering conditions and consequent differences in microstructures and sum of cracks (25).

Our study showed that aging had no adverse effect on FS of zirconia specimens. This result has also been confirmed by several previous studies (26). In a study by Papanagiotou *et al.*, in 2006, the process of thermal aging at low temperatures had no negative effect on FS of Y-TZP ceramics cut from In-Ceram YZ ceramic blocks (26). Ardlin (2002) demonstrated that FS of Y-TZP high-strength ceramics was not influenced by the process of thermal aging at low temperatures or chemical aging (immersion in 4% citric acid for 168 hours at 80°C) (27). In a study by Picconi, *et al.* (1998) zirconia specimens were stored in Ringer's solution at 37°C for different time periods and after one year no change occurred in the FS of specimens. In their study, hydrothermal procedures at 120°C for 120 hours in a humid environment had limited effects on the FS of Y-TZP ceramic specimens (28).

Yilmaz *et al.* in 2011 evaluated the effect of aging on FS of Lava and Cercon zirconia ceramics (22). In their study, specimens were subjected to 20,000 cycles of 200N load with 2Hz frequency and no significant difference was noted in the FS of aging and no aging groups. Vult Von Steyern *et al.* (1993) assessed the effect of 10,000 mechanical cycles and 5000 thermal cycles on FS of specimens (23) and reported no significant difference in FS of specimens with and without aging.

Pittayachawan *et al.* (2007) and Curtis *et al.* (2006) calculated the FS of Lava zirconia with

and without mechanical cycles (10,000 and 20,000 cycles at 250N, 2000 cycles at 500N, 700N and 800N and 10,000 and 100,000 cycles at 80N load, respectively) and reported no significant effect on zirconia strength (21, 29).

In a study by Brochers *et al.* (2010), the effects of different environments and loading conditions on the FS of In-Ceram YZ and Lava zirconia specimens were evaluated. Mechanical loading with 100N stress for 1 and 5 million cycles, thermocycling for 10,000 cycles and storage in distilled water at 36°C for 200 days, 80°C for 64 days and 134°C for 8 hours were found to have no significant effect on zirconia strength (25).

It appears that zirconia is resistant to aging during functional loading cycles for at least 75 months with 800,000 masticatory cycles per year (11). In other words, this level of aging during this time period cannot cause zirconia destruction (29).

In our study, similar to many previous ones, aging had no significant effect on FS. However, some others have reported reduction in FS of zirconia ceramics. If the phase transformation does not continue into the material mass, the FS would not decrease significantly. In other words, transformation of tetragonal to monoclinic phase starts at the material surface and propagates inward. This phase transformation at the surface is associated with increased volume but does not cause significant internal stress. Only after formation of a significant amount of monoclinic phase on the surface, stresses may accumulate and cause microcracks. When microcracks reach adequate length, they can cause fracture and decrease the strength of the ceramic (25). This case scenario did not occur in any of our understudy specimens.

Kim *et al.* in 2009 investigated the effects of aging at low temperatures on mechanical properties and phase stability of Y-TZP ceramics and reported that these effects were influenced by the temperature at which the specimens were stored (30). Chevalier *et al.* (1999) reported that

by increased temperature and duration of aging, the rate of phase transformation increased and this issue was related to the size of grains (8). Simultaneous with an increase in tetragonal grain, the stable phase gradually disappears. In the current study, the FS of zirconia groups increased following the process of aging. Theoretically, aging at 134°C for one hour corresponds to 3-4 years of clinical service (31, 32). Itinoche *et al.* (2006) measured the FS of In-Ceram zirconia with and without mechanical cycles (20,000 cycles at 50N load) and demonstrated that mechanical cycles decreased the FS of specimens; however, this reduction was not statistically significant (24).

Chevalier *et al.* (1999) indicated that as the result of aging at 130°C for 7 hours, for a monoclinic content higher than 30%, the rate of nucleation reached the saturation level (13). Thus, one possible explanation for increased FS may be the concentration of the monoclinic phase. The transformation of tetragonal to monoclinic phase starts at the surface of zirconia specimens. As long as the monoclinic phase is limited to a small area on the surface, changes in grain size and physical properties are insignificant (21). On the other hand, residual stresses are eliminated and the expansion created by the phase transformation prevents crack propagation (6). This process may be related to the increased FS of specimens. On the other hand, when the saturation phenomenon occurs at the surface of zirconia in the monoclinic phase, the transformation phase occurs in the body of ceramic. In this situation, internal cracks may occur in the critical zone and cause inevitable reduction in FS (6).

Vásquez *et al.* (2008) investigated the effects of mechanical and thermal cycling on FS of glass ceramics fused to titanium and reported that application of mechanical and thermal cycles decreased the FS of specimens in comparison with the control samples (31).

Att *et al.* (2007) compared the FS of Vita YZ,

Cerec In-Lab and Procera specimens with and without aging. Specimens in the aging group were subjected to 120,000 thermo-mechanical cycles (corresponding to 5 years of clinical service) with 49N force, which resulted in a reduction in strength of specimens particularly in the Procera group (32).

The controversial results obtained by different studies may be due to the different aging processes or type of strength testing. Density of presintered zirconia blocks (due to correlation with critical crack size), the sinterability of the powder (due to correlation with the size of primary grains), mechanically created cracks, residual compressive stresses during the preparation of specimens and the yttria content (due to its significance in transition of tetragonal to monoclinic phase) also play a role in ceramic strength.

Previous studies on the phase stability of zirconia ceramics mostly showed no reduction in strength as the result of aging. Tinschert in 2000 and Tanaka in 2003 reported that zirconia ceramics fabricated in early 1980 were less stable than the currently used Y-TZP ceramics (33, 34). Moreover, it appears that standard Y-TZP ceramics with high density and adequate concentration of Yttria did not experience any reduction in strength related to phase transformation even after long-term clinical service. Also, researchers reported that commercial Y-TZP ceramics still had adequate stability after being subjected to long-term clinical and experimental aging procedures and no aging-related mechanical destruction was noted (35). The results of the current study regarding no significant change in FS of Zirkozahn and Mamut specimens following aging was in accord with the findings of previous studies (27, 35).

### **Conclusion:**

Aging had no significant effect on TPFS of

Zirkonzahn and Mamut zirconia ceramics. Thus, they seem to have adequately high strength for application in the clinical setting and they are expected to show favorable results in long-term

clinical service. However, clinical studies are required to cast a definite judgment in this respect.

**Conflict of interest: “None Declared”**

## References:

1. Denry I, Kelly JR. State of the art of zirconia for dental applications. *Dent Mater* 2008; 24: 299-307.
2. Cattani-Lorente M, Scherrer SS, Ammann P, Jobin M, Wiskott HW. Low temperature degradation of a Y-TZP dental ceramic. *Acta Biomater* 2011; 7: 858-865.
3. Guo X. On the degradation of zirconia ceramics during low-temperature annealing in water or water vapor. *J Physics Chem Solids* 1999; 60: 539-546.
4. Kawai Y, Uo M, Wang Y, Kono S, Ohnuki S, Watari F. Phase transformation of zirconia ceramics by hydrothermal degradation. *Dent Mater J* 2011; 30: 286-292.
5. Lawson S. Environmental degradation of zirconia ceramics. *J Eur Ceram Soc* 1995; 15: 485-502.
6. Miyazaki T, Nakamura T, Matsumura H, Ban S, Kobayashi T. Current status of zirconia restoration. *J Prosthodont Res* 2013; 57: 236-261.
7. Sanon C, Chevalier J, Douillard T, Kohal RJ, Coelho PG, Hjerpe J *et al.* Low temperature degradation and reliability of one-piece ceramic oral implants with a porous surface. *Dent Mater* 2013; 29: 389-397.
8. Chevalier J, Olagnon C, Fantozzi G. Subcritical crack propagation in 3Y-TZP ceramics: static and cyclic fatigue. *J Am Ceram Soc* 1999; 82: 3129-3138.
9. Studart AR, Filser F, Kocher P, Gauckler LJ. *In vitro* lifetime of dental ceramics under cyclic loading in water. *Biomaterials* 2007; 28: 2695-2705.
10. Addison O, Fleming GJ, Marquis PM. The effect of thermocycling on the strength of porcelain laminates veneer (PLV) materials. *Dent Mater* 2003; 19: 291-297.
11. Rosentritt M, Behr M, Gebhard R, Handel G. Influence of stress simulation parameters on the fracture strength of all-ceramic fixed-partial dentures. *Dent Mater* 2006; 22: 176-182.
12. Muñoz-Saldanã J, Balmori-Ramirez H, Jaramillo-Vigueras D, Iga T, Schneider GA. Mechanical properties and low-temperature aging of tetragonal zirconia polycrystals processed by hot isostatic pressing. *J Mater Res* 2003; 18: 2415-2424.
13. Chevalier J, Cales B, Drouin JM. Low-temperature aging of Y-TZP ceramics. *J Am Ceram Soc* 1999; 82: 2150-2154.
14. Deville S, Chevalier J, Gremillard L. Influence of surface finish and residual stresses on the ageing sensitivity of biomedical grade zirconia. *Biomaterials* 2006; 27: 2186-2192.
15. Gremillard L, Epicier T, Chevalier J, Fantozzi G. Microstructural study of silica-doped zirconia ceramics. *Acta Mater* 2000; 48: 4647-4652.
16. Tsubakino H, Nozato R, Hamamoto M. Effect of alumina addition on the tetragonal-to-monoclinic phase transformation in zirconia- 3 mol % Yttria. *J Am Ceram Soc* 1991; 74: 440-443.
17. Boutz MMR, Winnubst AJA, Van Langerak B, Oldescholtenhuis RJM, Kreuwel K, Burggraaf AJ. The effect of ceria codoping on chemical stability and fracture toughness of Y-TZP. *J Mater Sci* 1995; 30: 1854-1862.
18. Hernandez MT, Jurado JR, Duran P, Fierro JLG. Subeutectoid degradation of yttria-stabilized tetragonal zirconia polycrystal and ceria-doped yttria-stabilized tetragonal zirconia polycrystals

- ceramics. *J Am Ceram Soc* 1991; 74: 1254-1258.
19. Studart AR, Filser F, Kocher P, Gauckler LJ. Fatigue of zirconia under cyclic loading in water and its implications for the design of dental bridges. *Dent Mater* 2007; 23: 106-114.
  20. Yoshinari M, Dérand T. Fracture strength of all-ceramic crowns. *Int J Prosthodont* 1994; 7: 329-338.
  21. Pittayachawan P, McDonald A, Petrie A, Knowles JC. The biaxial flexural strength and fatigue property of Lava Y-TZP dental ceramic. *Dent Mater* 2007; 23: 1018-1029.
  22. Yilmaz H, Nemli SK, Aydin C, Bal BT, Tiras T. Effect of fatigue on biaxial strength of bilayered porcelain/zirconia (Y-TZP) dental ceramics. *Dent Mater* 2011; 27: 786-795.
  23. Vult Von Steyern P, Ebbesson S, Holmgren J, Haag P, Nilner K. Fracture strength of two oxide ceramic crown systems after cyclic pre-loading and thermocycling. *J Oral Rehabil* 2006; 33: 682-689.
  24. Itinoche KM, Ozcan M, Bottino MA, Oyafuso D. Effect of mechanical cycling on the flexural strength of densely sintered ceramics. *Dent Mater* 2006; 22: 1029-1034.
  25. Borchers L, Stiesch M, Bach FW, Buhl JC, Hubsch C, Kellner T, *et al.* Influence of hydrothermal and mechanical conditions on the strength of zirconia. *Acta Biomater* 2010; 6: 4547-452.
  26. Papanagiotou HP, Morgano SM, Giordano RA, Pober R. *In vitro* evaluation of low-temperature aging effects and finishing procedures on the flexural strength and structural stability of Y-TZP dental ceramics. *J Prosthet Dent* 2006; 96: 154-164.
  27. Ardlin BL. Transformation-toughened zirconia for dental inlays, crowns and bridges: chemical stability and effect of low temperature aging on flexural strength and surface structure. *Dent mater* 2002; 18: 590-595.
  28. Piconi C, Burger W, Richter HG, Cittadini A, Maccauro G, Covacci BV, *et al.* Y-TZP ceramics for artificial joint replacements. *Biomaterials* 1998; 19: 1489-1494.
  29. Curtis AR, Wright AJ, Fleming GJ. The influence of simulated masticatory loading regimes on the bi-axial flexure strength and reliability of a Y-TZP dental ceramic. *J Dent* 2006; 34: 317-325.
  30. Kim HT, Han JS, Yang JH, Lee JB, Kim SH. The effect of low temperature aging on the mechanical property & phase stability of Y-TZP ceramics. *J Adv Prosthodont* 2009; 1: 113-117.
  31. Vásquez V, Ozcan M, Nishioka R, Souza R, Mesquita A, Pavanelli C. Mechanical and thermal cycling effects on the flexural strength of glass ceramics fused to titanium. *Dent Mater J* 2008; 27: 7-15.
  32. Att W, Grigoriadou M, Strub JR. ZrO<sub>2</sub> three-unit fixed partial dentures: comparison of failure load before and after exposure to mastication simulator. *J Oral Rehabil* 2007; 34: 282-290.
  33. Tinschert J, Zvez D, Marx R, Anusavice KJ. Structural reliability of alumina-, feldspar-, leucire-, mica- and zirconia-based ceramics. *J Dent* 2000; 28: 529-535.
  34. Tanaka K, Tamura J, Kawanabe K, Nawa M, Uchida M, Kukubo T, *et al.* Phase stability after aging and its influence on pin-on-disk wear properties of Ce-TZP/Al<sub>2</sub>O<sub>3</sub> nanocomposite and conventional Y-TZP. *J Biomed Mater Res A* 2003; 67: 200-207.
  35. Guazzato M, Albakry M, Ringer SP, Swain MV. Strength, fracture toughness and microstructure of a selection of all-ceramic materials. Part II. Zirconia-based dental ceramics. *Dent Mater* 2004; 20: 449-456.